

Field study and regression modeling on soil water distribution with mulching and surface or subsurface drip irrigation systems

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Abstract: The soil water status was investigated under soil surface mulching techniques and two drip line depths from the soil surface (D_L). These techniques were black plastic film (BPF), palm tree waste (PTW), and no mulching (NM) as the control treatment. The D_L were 15 cm and 25 cm, with surface drip irrigation used as the control. The results indicated that both the BPF and PTW mulching enhanced the soil water retention capacity and there was about 6% water saving in subsurface drip irrigation, compared with NM. Furthermore, the water savings at a D_L of 25 cm were lower (15-20 mm) than those at a D_L of 15 cm (19-24 mm), whereas surface drip irrigation consumed more water. The distribution of soil water content (θ_v) for BPF and PTW were more useful than for NM. Hence, mulching the soil with PTW is recommended due to the lower costs and using a D_L of 15 cm. The θ_v values were derived using multiple linear regression (MLR) and multiple nonlinear regression (MNL) models. Multiple regression analysis revealed the superiority of the MLR over the MNL model, which in the training and testing processes had coefficients of correlation of 0.86 and 0.88, root mean square errors of 0.37 and 0.35, and indices of agreement of 0.99 and 0.93, respectively, over the MNL model. Moreover, D_L and spacing from the drip line had a significant effect on the estimation of θ_v .

Keywords: palm tree waste mulching, plastic film mulching, soil water distribution, regression models

DOI: 10.25165/ijabe.20211402.5200

Citation: Mattar M A, Al-Othman A A, Elansary H O, Elfeky A M, Alshami A K. Field study and regression modeling on soil water distribution with mulching and surface or subsurface drip irrigation systems. *Int J Agric & Biol Eng*, 2021; 14(2): 142–150.

1 Introduction

In arid regions, such as Saudi Arabia, the absence of an effective water management system results in high water loss during irrigation^[1]. The climate is also hyper arid, with these factors having a big effect on the limited water supplies and agriculture^[2]. Therefore, drip irrigation has been adopted, as it is assumed to be the foremost efficient and valuable source for stabilizing the utilization of water in comparison with other systems. Surface drip irrigation (DI) often decreases water loss due to less water evaporation and deep percolation^[1]. Despite these advantages, there are also several disadvantages of applying DI, including the possibility of damage, direct exposure of the drip lines to the sun, and the occurrence of salinity. Thus, subsurface drip irrigation (SDI) has been proposed as a more useful method

because it uses less water than DI because of reduced evaporation from the soil surface^[3,4]. SDI is often used to control the quantity of water applied without having any significant environmental damage as a result of flow elimination and deep penetration^[5]. Overall, this method reinforces the production of crops by decreasing water waste^[6-8]. SDI is more effective than DI because it provides water directly to the root zone^[9]. However, this system's performance can be affected depending on the space between the emitters and the lined depth of the drip lines^[7].

Some precautionary measures should be taken in the SDI system for crop production. According to Enciso et al.^[7], there should be suitable spacing between emitters, taking into account the depth and type of drip lines during the design process to enhance irrigation efficiency and increase productivity^[10]. Magwenzi^[11] stated that the depth of the drip lines can vary from 10 to 20 cm. Several studies have been conducted on SDI in different crops. Najafi^[12] studied the effect of drip line depths of 15 and 30 cm on tomato crop yield. He found that the best yield was obtained at a drip line depth of 15 cm. In contrast, Zhuge et al.^[13] found that a drip line depth of 30 cm provided better root distribution and nutrient absorption in tomato cultivation than at depths of 20 and 40 cm. Patel and Rajput^[14] found that a drip line depth of 10 cm was best with 60.7 cm of irrigation water applied when planting onions in sandy, loamy soil. Al-Harbi et al.^[15] also found that using a drip line of 35 cm improved growth and reduced evaporation from the soil surface. A study by Douh and Boujelben^[16] showed that the soil water content was recorded up to a depth of 80 cm from the surface in drip lines of 15 cm used to

Received date: 2019-06-13 **Accepted date:** 2020-10-14

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produce eggplant and the water saving was 23.2% higher than that of the DI system. Moreover, the soil profile of the water distribution was more constant in the SDI system than the DI system. Çolak et al.^[17] revealed that evaporation losses were lower in SDI receiving slightly less water than the DI in eggplant. In addition, Al-Ghobari and Dewidar^[18] reported that the soil water contents in SDI were higher than those in DI during the tomato growth stages. Further, Pisciotta et al.^[19] used drip lines at a depth of 35 cm to prevent damage from tillage during the cultivation of grapevines.

In the field of agriculture, several techniques other than SDI, such as soil surface mulching, have been explored to improve water absorption^[20]. These techniques are commonly used to avoid evaporation loss from the soil surface and enhance crop growth environments to increase crop yields^[6,21-25]. One soil surface mulching technique that has been used in recent years is crop straw, which minimizes soil water evaporation, ameliorates the soil's physical and chemical properties, and promotes biological activity^[26-29]. In maize cultivation, Li et al.^[23,24] found that straw mulching saved about 35% of water during the growth stages. Plastic film mulching is a well-evolved technique that is currently being used for cultivation, especially in areas where irrigation water is scarce^[30]. It has been shown to enhance thermal conditions and increase water storage in the upper soil layers^[31,32], improving crop growth and water productivity^[33,34]. In some cases, an SDI system mulched with plastic film is used to increase vegetable production^[35], for example, Zotarelli et al.^[36] and Baghani et al.^[37]. Wang et al.^[38] and Ma et al.^[39] reported that using plastic film mulching increased the yield of maize and potato in semiarid regions by maintaining soil moisture in the upper layers.

A combination of SDI and mulching can possibly reduce soil

water evaporation in an arid environment. Therefore, this study aimed to (1) explore the status of the volumetric soil water content (θ_v) under different drip line depths and soil surface mulching using black plastic film (BPF) and palm tree waste (PTW), (2) develop empirical models using multiple regression analyses to estimate the θ_v values for soil profiles under an SDI for different mulching to study important parameters affecting θ_v .

2 Materials and methods

2.1 Field conditions and experimental design

The experiment was conducted at the Agricultural Research Farm in Dirab, Riyadh (24.4195°N, 46.65°E, and 552 m a.s.l.) during the summer months of 2018. Climatic data were recorded as monthly averages during the experimental period (June, July, August, and September) as follows: 36.6 °C, 37.4 °C, 35.8 °C, and 34.6 °C, respectively, for air temperatures; 10.1%, 11.8%, 13.7%, and 13.5%, respectively, for relative humidity; 5.6 m/s, 6.1 m/s, 6.6 m/s, and 5.6 m/s, respectively, for maximum wind speed; and 24.7 MJ/m² d, 24.8 MJ/m² d, 23.4 MJ/m² d, and 23.2 MJ/m² d, respectively, for solar radiation. Moreover, there was no rainfall during these months.

The field experiments were planned and implemented, as shown in Figure 1. The DI system was designed using a water tank, pump, pressure gauges, pressure regulators, flow meter, ball relief, solenoid valves, main lines, sub-mains, and drip lines. A 5000 L water tank was used in the irrigation network. The drip lines (16 mm inner diameter and 1 mm thickness) were placed at the soil surface (i.e., DI) and two depths from the soil surface (D_1) of 15 cm and 25 cm. The emitters had a discharge rate of 4 L/h at 150 kPa operating pressure with a spacing of 30 cm on the drip line. Two soil surface mulches, BPF and PTW, were applied, as well as

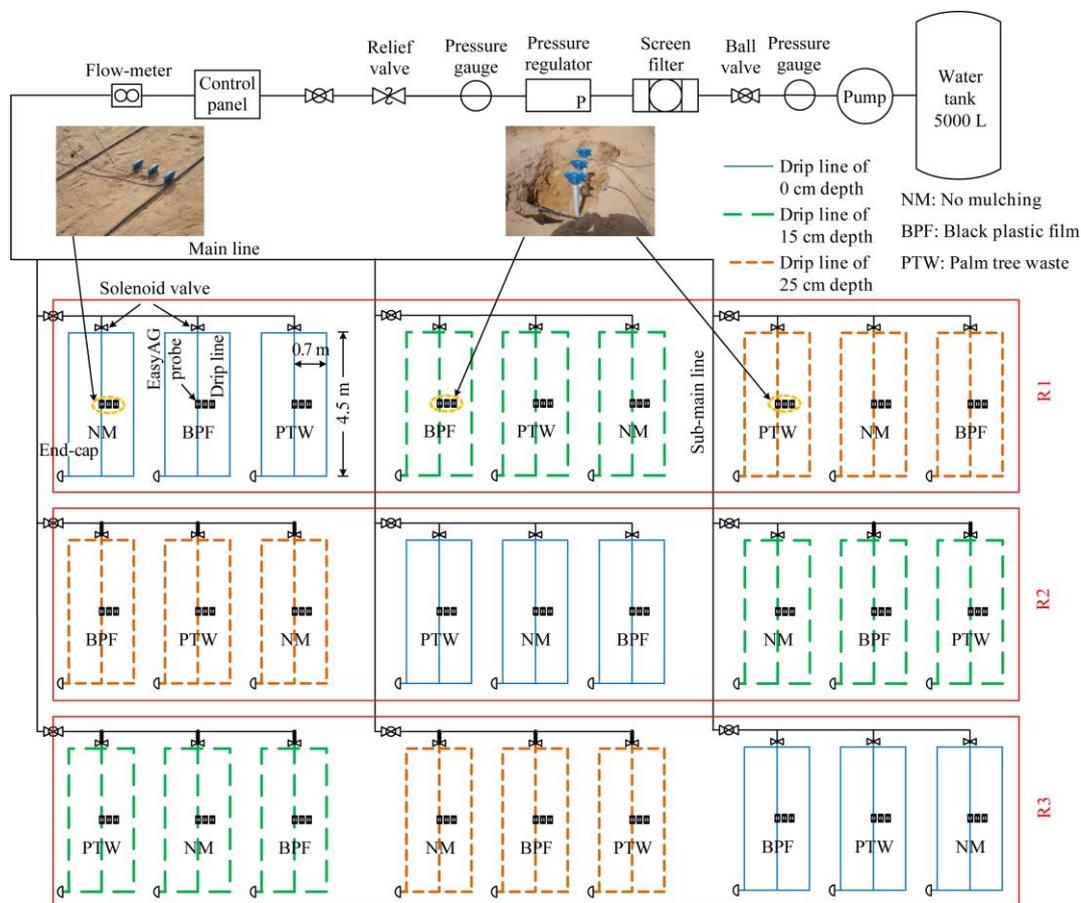


Figure 1 Experimental layout

no mulching (NM). A randomized complete block design was used with three replications (Figure 1). Before conducting the experiments, three soil samples were collected from different depths to determine physical and chemical properties (see Table 1).

Three samples of irrigation water were also analyzed to determine their chemical properties, which were an electrical conductivity value of 4.5 dS/cm, pH 7.48, and total dissolved solids of 2880 mg/kg.

Table 1 Physical and chemical properties of soil samples from the experimental site

Soil depth /cm	Particle size distribution/%			Soil texture	Physical properties					Chemical properties				
	Clay	Silt	Sand		θ_i /%	FC/%	WP/%	ρ_b /g cm ⁻³	EC/dS m ⁻¹	pH	CaCO ₃	Na	K	P
Plot 1														
0-25	3.2	22.5	74.3	Loamy sand	1.22	14.58	3.04	1.51	1.47	7.85	25.54	61	116	31.1
25-50	3.2	22.5	74.3	Loamy sand	1.36	15.99	3.39	1.41	2.4	7.73	27.04	181	115	21.8
Plot 2														
0-25	3.2	15	81.8	Loamy sand	1.22	14.86	3.05	1.52	3.4	7.8	25.37	237	109	12.5
25-50	1.95	16.25	81.8	Loamy sand	1.15	15.15	2.45	1.40	2.37	7.87	24.75	139	110	9.3
Plot 3														
0-25	4.45	16.25	79.3	Loamy sand	1.37	17.57	3.05	1.50	3.09	7.81	24.75	330	81	24.9
25-50	0.7	12.5	86.8	Sand	0.93	14.81	2.06	1.40	2.05	7.91	23.34	218	70	34.2

Note: Plot 1: drip line depth = 0 cm; Plot 2: drip line depth = 15 cm; Plot 3: drip line depth = 25 cm; θ_i : Initial water content; FC: field capacity; WP: Wilting point; ρ_b : Soil bulk density; EC: Electrical conductivity.

2.2 Irrigation water

An irrigation schedule was applied using soil sensors to continuously monitor the θ_v and supply a suitable amount of irrigation water to the planned irrigation treatment. Its purpose was to maximize the irrigation efficiency by applying the appropriate amount of water needed to replenish the soil water to the desired level at field capacity (FC). However, no crops were planted in this study. Therefore, the depth of water applied to reach the FC (D_w) was calculated for a soil depth (D) of 50 cm at increments of 10 cm using Equation (1):

$$D_w = \sum_{i=1}^n D_i (FC_i - \theta_{vi}) \tag{1}$$

where, D_w is the depth of water applied to reach the field capacity, mm; n is the number of sensors; D_i is the soil depth at the i^{th} sensor, mm; FC_i is the field capacity of the soil at the i^{th} sensor; and θ_{vi} is the soil water content at the i^{th} sensor.

2.3 Monitoring soil water content

Three EasyAG probes (Sentek Sensor Technologies, Stepney, Australia), including several sensors (electrical capacitance) were used and installed in each plot to monitor the values of θ_v at a soil depth from 10 to 50 cm. These probes were placed as follows: the first was placed directly at the emitter, the second was placed at a 15 cm spacing from the drip line (S), and the third was at S of 30 cm, as shown in Figure 1.

The electrical capacitance from the probe recorded a scaled frequency reading (SF) in the field to provide a θ_v using a calibration equation, as follow:

$$SF = \frac{(F_A - F_S)}{(F_A - F_W)} \tag{2}$$

$$\theta_v = \left(\frac{SF - C}{A} \right)^{\frac{1}{B}} \tag{3}$$

where, F_A , F_S , and F_W are frequency readings in the air, soil, and water, respectively, and A , B , and C are constants obtained from calibration procedure of the probes (Table 2).

Table 2 Constants of Equation (3) for three sensors after calibration

Sensor location	A	B	C	R ²
Directly on drip line	60.619	0.109	-71.356	0.942
At spacing of 15 cm from drip line	476.132	0.014	-485.695	0.844
At spacing of 30 cm from drip line	507.365	0.011	-513.789	0.751

2.4 Multiple regression analysis

The multiple linear regression (MLR) and multiple nonlinear regression (MNL) models were derived using the data acquired from the field experiment. The dependent variable is estimated when the values of the independent variables are obtained from the linear and nonlinear combinations in a multiple regression model. Based on the results of the MLR and MNL, the effects of the influencing factors on θ_v can be better explained. The corresponding model expressions can be described as follows:

MLR model:

$$\hat{Y} = a_0 + a_1 X_1 + a_2 X_2 + a_3 X_3 + \dots + a_m X_m \tag{4}$$

where, \hat{Y} is the predicted value of the dependent variable, a_i ($i = 0, \dots, m$) are the estimated regression coefficients for the linear relation, and X_i ($i = 1, \dots, m$) are the independent variables.

MNL model:

$$\hat{Y} = b_0 \times X_1^{b_1} \times X_2^{b_2} \times X_3^{b_3} \times \dots \times X_m^{b_m} \tag{5}$$

where, b_i ($i = 0, \dots, m$) are the estimated regression coefficients for the nonlinear relation.

The regression models were developed, and the mulching types (MT) that were categorized as 0 for NM, 2 for BPF, and 3 for PTW, D_L , S , and D were considered as independent variables, whereas θ_v was the dependent variable. In the present study, 135 data points were used to derive all regression models. The models were developed using 60% of the data for the training process, and 20% of the data were used to test the models. The remaining data were used for model validation. During the validation process, the performance of the developed regression models were checked under NM, BPF, and PTW. The statistical characteristics of θ_v data for each process are provided in Table 3. The SPSS Statistics software package (version 16.0; SPSS; Chicago, IL, USA) was used to perform the regression analysis.

Statistical performance evaluation criteria were calculated to test the goodness of fit of the regression models during the training, testing, and validation processes. The criteria utilized were the coefficients of correlation (r), root mean square errors (RMSE), and index of agreement (IA). r measured the degree of correlation between the measured and calculated θ_v values with values close to 1.0 indicating a perfect agreement, and it was calculated as follows:

$$r = \frac{\sum_{i=1}^N (M_i - \bar{M})(C_i - \bar{C})}{\sqrt{\sum_{i=1}^N (M_i - \bar{M})^2 \sum_{i=1}^N (C_i - \bar{C})^2}} \tag{6}$$

where, M_i is the measured value; C_i is the calculated value; N is the number of data; \bar{M} is the average measured value; and \bar{C} is the average calculated value; $RMSE$ expresses the error in the same units as the variable^[40] and measures the difference between the calculated and measured values^[41] by:

$$RMSE = \sqrt{\frac{\sum_{i=1}^N (M_i - C_i)^2}{N}} \quad (7)$$

IA represents the ratio between the mean square error and the potential error, as defined by Willmot^[42]:

$$IA = 1 - \frac{\sum_{i=1}^N (M_i - C_i)^2}{\sum_{i=1}^N (|C_i - \bar{M}| + |M_i - \bar{M}|)^2} \quad (8)$$

IA has a range from 0 to 1, with a perfect fit at 1^[40].

Table 3 Statistical parameters of θ_v data used for the training, testing, and validation processes

	X_m	X_d	X_n	S_x	K_x	C_{sx}
Training process	15.60	14.17	12.28	0.723	-0.291	-0.010
Testing process	15.36	13.98	12.45	0.708	-0.123	-0.030
Validation process						
NM	14.81	13.75	12.58	0.784	-0.799	-0.410
BPF	15.32	14.05	13.10	0.820	-1.134	0.585
PTW	15.29	14.13	12.97	0.771	-1.132	-0.028

Note: X_m : maximum value; X_d : mean value; X_n : minimum value; S_x : standard deviation; K_x : kurtosis coefficient; C_{sx} : skewness coefficient; NM: no mulching; BPF: black plastic film; PTW: palm tree waste.

2.5 Statistical analysis

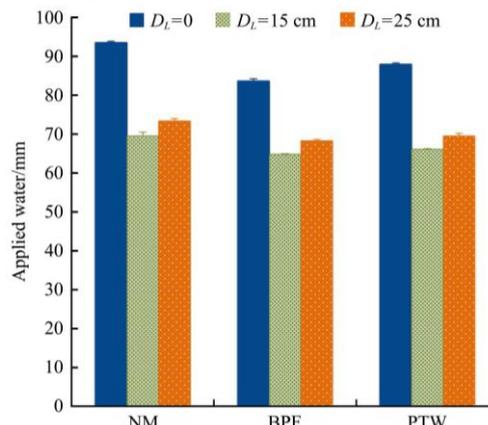
An analysis of variance was performed using CoStat version 6.303 (CoStat Version 6.303 Copyright 1998-2004) to determine the effects of D_L and MT on the measured θ_v . The treatment means were separated using a least significant difference test at $p = 0.05$.

3 Results and discussion

3.1 Applied water

The BPF treatment achieved water savings of 10.55%, 6.79%, and 7.02% at D_L of 0 cm, 15 cm, and 25 cm, respectively, compared with the NM treatment, which had 93.5 mm, 69 mm, and 73 mm of applied water, respectively, while the PTW treatment achieved water savings of 5.96%, 4.94%, and 5.26%, respectively (Figure 2). The water applied under DI, at a D_L of 0 cm, with any type of mulching was conserved less than that applied under SDI, at a D_L of 15 or 25 cm, where soil surface evaporation rates were high^[4,43]. Additionally, as shown in Figure 2, using BPF or PTW above a D_L of 25 cm required the application of more water than a

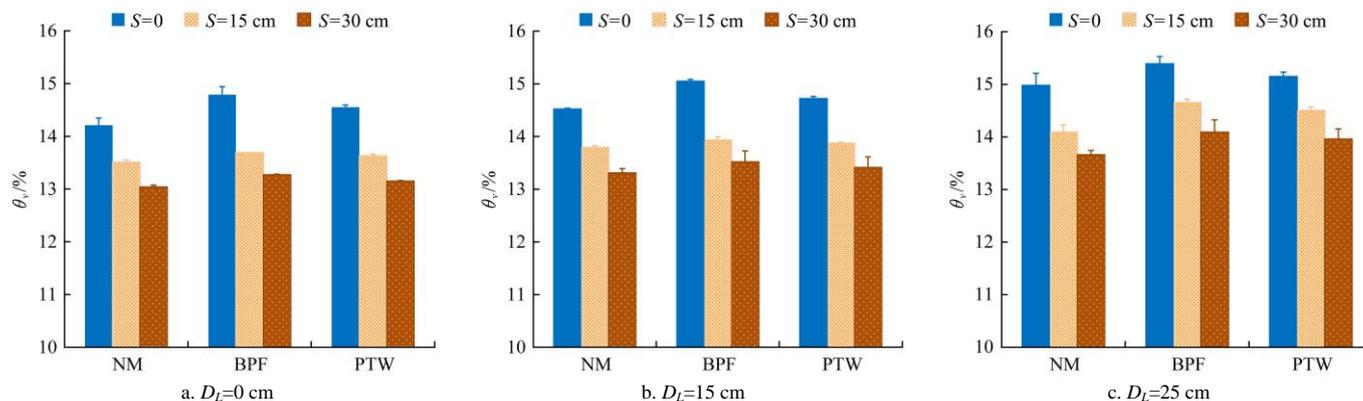
D_L of 15 cm. Therefore, the use of SDI with BPF or PTW mulching retained soil moisture and decreased the amount of water required^[44]. Thus, it is preferable to use PTW mulching at a D_L of 15 cm, as there are fewer additional costs.



Note: NM: no mulching; BPF: black plastic film; PTW: palm tree waste. Figure 2 Water applied under different mulching types at different drip line depths from the soil surface (D_L)

3.2 Effect of mulching type on soil water content

Regardless of the D_L treatments, Tables 5 shows that there were significant effects of MT on θ_v values at different S . The average θ_v values for the BPF treatment were the highest, followed by the PTW treatment in both drip systems (Figure 3). For the D_L of 0 cm with BPF mulching at S of 0, 15, and 30 cm, the θ_v values increased by 4.08%, 1.33%, and 1.76%, respectively, compared with the NM treatment, while there were increases of 2.39%, 0.89%, and 0.84%, respectively, with PTW mulching (Figure 3). For a D_L of 15 cm, the BPF and PTW treatments at an S of 0 cm had θ_v values that were 3.65% and 1.38% higher, respectively, than those of the NM treatment, while there were increases of 1.02% and 0.58%, respectively, at an S of 15 cm and increases of 1.58% and 0.75%, respectively, at an S of 30 cm (Figure 3). For a D_L of 25 cm, there were increases of 2.74% and 1.13%, respectively, in the θ_v values at an S of 0 cm for the BPF and PTW treatments compared with the NM treatment. Additionally, the corresponding values of the BPF and PTW treatment increased by 3.97% and 2.91%, respectively, at an S of 15 cm and by 3.15% and 2.20%, respectively, at an S of 30 cm (Figure 3). The use of BPF or PTW mulching substantially limits the flux of water vapor from the soil surface into the air^[23,24,45,46]. Although the purchase cost of BPF is high, it can be replaced by PTW, which is available at no additional cost.



Note: NM: no mulching; BPF: black plastic film; PTW: palm tree waste. Figure 3 Average soil water content (θ_v) under different spacing from drip line (S) and mulching types at different drip line depths from the soil surface (D_L)

3.3 Effect of the depth of the drip line on soil water content

Regardless of the mulching treatments, the D_L significantly affected ($p < 0.01$) the average θ_v values at different S (Table 4), with a D_L of 25 cm having the highest θ_v values, in contrast to a D_L of 0 cm. The average θ_v values for a D_L of 25 cm were highest at S of 0, 15, and 30 cm under the NM treatment, which increased by 3.17%, 2.18%, and 2.63% at a D_L of 15 cm, respectively, and increased by 5.42%, 4.29%, and 4.75%, respectively, at a D_L of 0 cm (Figure 3). These findings are consistent with findings by Mokh et al.^[47], who observed that θ_v values increased with increasing D_L . The θ_v values in the BPF and PTW treatments under different D_L showed a similar trend (Figure 3). For the BPF treatment, a D_L of 25 cm produced the highest θ_v values, which were 2.26% (at an S of 0 cm), 5.17% (at an S of 15 cm), and 4.22% (at an S of 30 cm) higher than the θ_v values at a D_L of 15 cm and 4.06%, 7.01%, and 6.18% higher, respectively, than the θ_v values at a D_L of 0 cm. For the PTW treatment, the θ_v values at a D_L of 25 cm were 2.92%, 4.54%, and 4.10% higher than those at a D_L of 15 cm at S of 0, 15, and 30 cm, respectively, while there were increases of 4.12%, 6.38%, and 6.16%, respectively, comparison with a D_L of 0 cm. A small difference in average θ_v values was observed between the D_L of 15 cm and D_L of 25 cm. Therefore, a D_L of 15 cm should be selected because of the lower drilling costs. Installing a drip line below the soil surface and not exposing it to the sun increases the θ_v value, as moisture is not lost^[48].

Table 4 Results of variance analysis of θ_v values under mulching type (MT) and drip line depth from the soil surface (D_L) at different spacing from the drip line (S)

Treatments	$S = 0$ cm	$S = 15$ cm	$S = 30$ cm
MT	**	**	*
No mulching	14.57 ^c	13.79 ^b	13.33 ^b
Black plastic film	15.08 ^a	14.09 ^a	13.63 ^a
Palm tree waste	14.81 ^b	13.99 ^a	13.51 ^{ab}
LSD _{0.05}	0.17	0.11	0.19
D_L	**	**	**
Surface drip	14.52 ^c	13.61 ^c	13.15 ^c
Subsurface drip at 15 cm depth	14.76 ^b	13.86 ^b	13.41 ^b
Subsurface drip at 25 cm depth	15.14 ^a	14.42 ^a	13.91 ^a
LSD _{0.05}	0.17	0.11	0.20
MT \times D_L	ns	*	ns

Note: ns: Non-significant; *: Significant at $p < 0.05$; **: Significant at $p < 0.01$. Mean values in columns followed with different letters are significantly different based on the least significant difference test at $p < 0.05$ (LSD_{0.05}).

3.4 Soil water distribution

Figures 4-6 illustrate the effects of MT and D_L on the θ_v ,

distribution throughout the soil profile. D_L of 15 and 25 cm had the best uniformity of θ_v distribution contour lines at different S . When S increased, the θ_v bulb's spread decreased, in agreement with Assouline^[49], Grabow et al.^[50], Badr^[51], Shirahatti et al.^[52], and Nasrabad et al.^[53]. Since the horizontal movement of water is limited in sandy soils, there should be close spacing between the emitters^[54]. In addition, the vertical movement was higher than the horizontal movement under the SDI system^[43,55,56].

There were significant effects of interactions between the MT and D_L on the θ_v values at an S of 15 cm (Table 4). For D_L of 0, 15, and 25 cm at a D of 0-20 cm, the θ_v values of BPF were increased by 0.96%, 3.05% and 5.56%, respectively, compared with NM, while the θ_v values of PTW were 1.25%, 2.91%, and 5.41%, higher respectively, in agreement with Wang et al.^[57] and Liu et al.^[58]. Ma et al.^[39] found that using plastic films significantly increased the θ_v by 12.9% at a D of 0-20 cm, compared with the traditional method. The use of either BPF or PTW mulching maintains water evaporation and encourages the movement of water into the topsoil layers, which enhances θ_v during the initial growth stage of crops^[44]. The surface soil layer has a lower θ_v (i.e., not completely wet) for SDI than DI, thereby reducing the soil evaporation in SDI^[48]. At the active root depth (0-40 cm) for most crops, the NM at an S of 15 cm had average θ_v values of 13.87% and 14.13% for D_L of 15 and 25 cm, respectively (Figure 4). In sandy soils, SDI enhances the water recovery capacity^[59], while in loamy soils, a $D_L > 10$ cm is recommended to prevent wetting of the soil surface during irrigation^[60]. The average θ_v corresponding values for BPF and PTW were 14.02% and 13.97%, respectively, at a D_L of 15 cm, and 14.63% and 14.54%, respectively, at a D_L of 25 cm (Figures 5 and 6). This increased θ_v of BPF and PTW treatments could be attributed to minimal soil water loss, which has an important role in crop management and growth^[61,62]. Ashrafuzzaman et al.^[63] reported that water in the form of fog fell into the topsoil layer due to the vapors formed by water trapped inside the mulch. Figures 4-6 show that when the D_L increased, a saturation bulb of θ_v distribution below emitters became more controllable moving downward, especially with BPF and PTW, which also changed the shape of the bulb from a circular shape to an ellipse. This is in agreement with Thorburn et al.^[64], who showed that SDI controls the amount of water and the spread of θ_v toward the soil surface. BPF at a D_L of 25 cm allowed slightly more θ_v downward movement than PTW (Figures 5 and 6). However, it is better to use PTW mulching at a D_L of 15 cm because of its lower installation cost, despite the slightly lower θ_v values than at a D_L of 25 cm for PTW mulching.

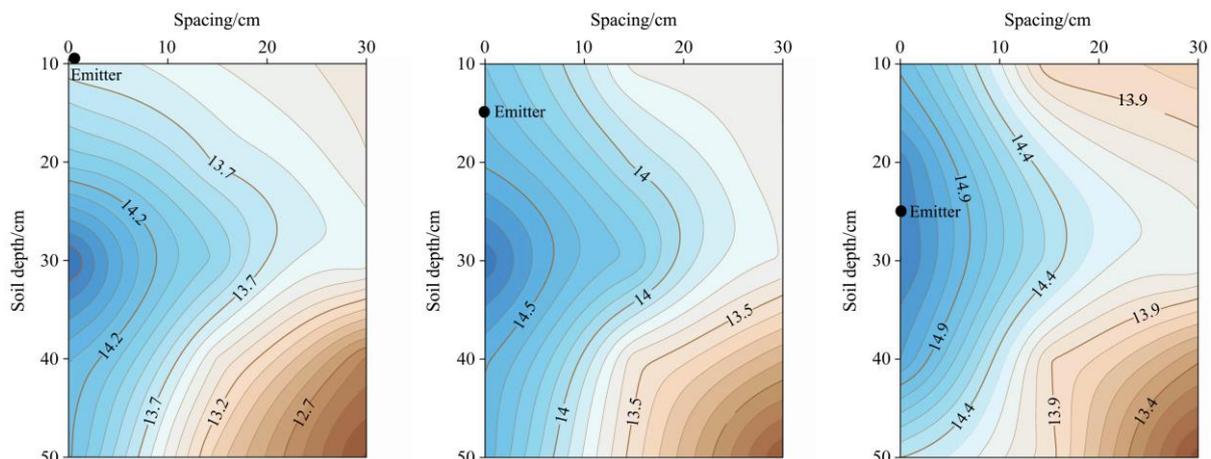


Figure 4 Soil water distribution through the emitter at different drip line depths under no mulching after irrigation for 24 h

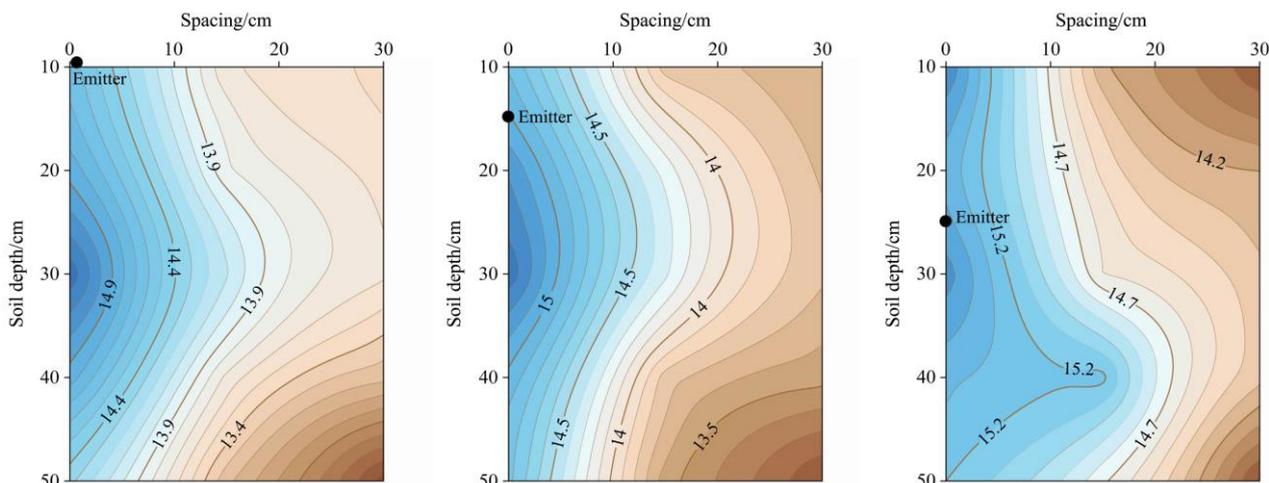


Figure 5 Soil water distribution through the emitter at different drip line depths under black plastic film mulching after irrigation for 24 h

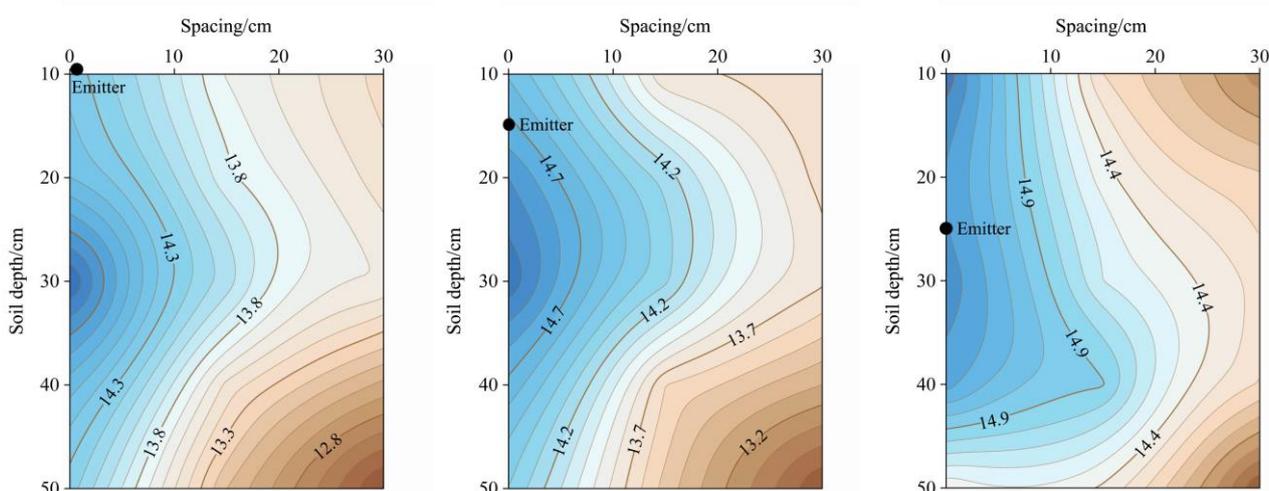


Figure 6 Soil water distribution through the emitter at different drip line depths under palm tree waste mulching after irrigation for 24 h

3.5 Performance of regression models

Important factors affecting θ_v values were identified using regression analyses that developed the mathematical models for θ_v , as given below:

For MLR

$$\theta_v = 14.58 + 0.071MT + 0.003D_L - 0.0089D - 0.047S \quad (9)$$

For MNLR

$$\theta_v = 15.24 \times MT^{0.004} \times D_L^{0.005} \times D^{-0.007} \times S^{-0.026} \quad (10)$$

Table 6 shows the standard error (SE), *t*-statistic (*t*-stat), probability (*p*-value), and variance inflation factor (VIF) for the independent variables (MT, D_L , *S*, and *D*) in the MLR model at a 95% confidence interval (CI). The *t*-stat values of the variables should be greater than 1.99 or less than -1.99 to confirm the goodness of fit of the regression coefficients. The *t*-stats of D_L and *S* were greater than 1.99 and less than -1.99, respectively. The *p*-values for the D_L and *S* were small ($p < 0.05$). The SE of the coefficients of D_L and *S* were 0.004. Therefore, D_L and *S* were the most significant variables in the calculation of θ_v . VIF values of all variables provided in Table 5 were equal to 1. There were no correlations between variables, which are expressive inputs in the MLR model. For the MNLR analysis at 95% CI, *M*, D_L , and *S* were more significant for θ_v , where CI did not include zero. The *D* was not significantly affected because the lower bound and upper bound of CI for *D* were -0.018 and 0.004, respectively.

Figure 7 shows the comparisons between the measured θ_v values and θ_v values calculated using the MLR and MNLR models when plotting the regression results of Equations (9) and (10) during

the training and testing processes. From the scatter plots, the MLR model provided the least scattered θ_v estimates whereas the MNLR model provided the worst results for the training and testing processes. Table 6 demonstrates the goodness of fit of each regression model during the training and testing processes. The *r* and *IA* values of the MLR model were higher and the *RMSE* value was lower than that of the MNLR model during the training process. The *r* and *IA* values for the MLR model were 2.87% and 9.06% higher, respectively, and the *RMSE* value was 6.87% lower than the values in the MNLR model. Based on the testing dataset, the trends of the MLR and MNLR model results were the same for the training dataset. The MLR model performed better than the MNLR model, with the *r* and *IA* values increasing by 3.53% and 2.64%, respectively, and the *RMSE* value decreasing by 8.97%.

Table 5 Standard error of regression coefficients, *t*-statistic, probability, and variance inflation factor of independent variables for the multiple linear regression model

	Intercept	Independent variables			
		MT	D_L	<i>S</i>	<i>D</i>
SE	0.135	0.034	0.004	0.004	0.003
<i>t</i> -stat	108.165	2.098	7.411	-13.110	-2.949
<i>p</i> -value	5.43×10^{-85}	0.039	1.46×10^{-10}	3.37×10^{-21}	0.004
VIF		1.00	1.03	1.02	1.00

Note: SE: standard error; *t*-stat: *t*-statistic; *p*-value: probability; VIF: variance inflation factor; MT: mulching types; D_L : drip line depth from the soil surface; *S*: spacing from drip line; *D*: soil depth.

Table 6 Statistical performance of the regression models during the training and testing processes

Statistical parameters	Training process		Testing process	
	MLR	MNLR	MLR	MNLR
r	0.861	0.837	0.879	0.849
$RMSE$	0.366	0.393	0.345	0.379
IA	0.987	0.905	0.934	0.910

Note: r : coefficients of correlation; $RMSE$: root mean square errors; IA : index of agreement.

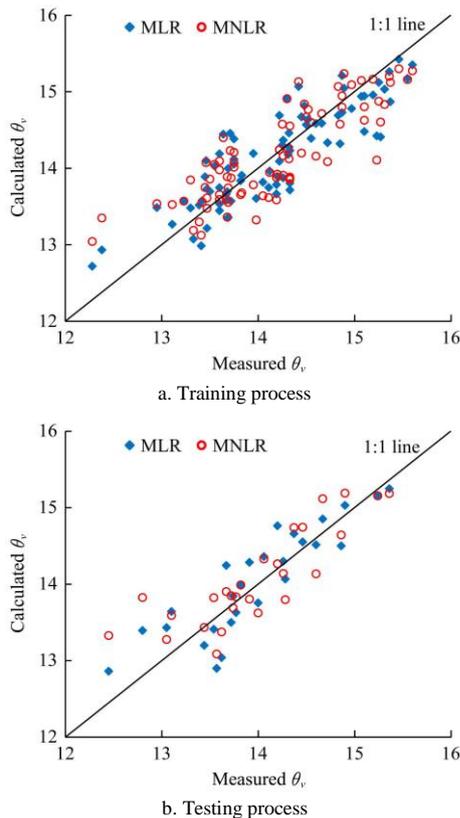
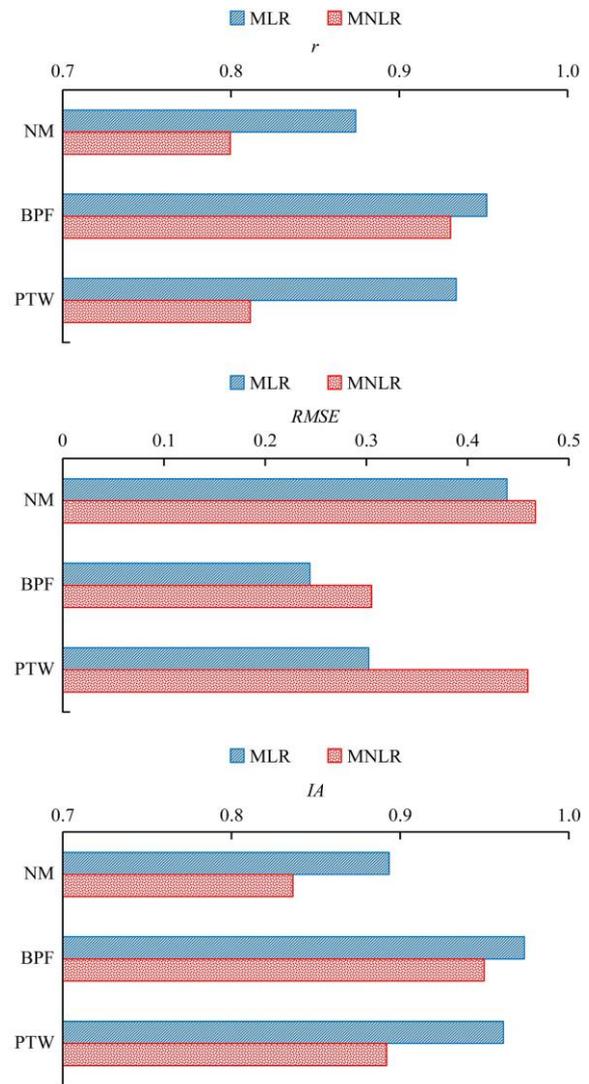


Figure 7 Scatterplots comparing measured θ_v values and θ_v values calculated by the multiple linear regression (MLR) and multiple nonlinear regression (MNLR) models

Figure 8 shows the statistical performance values of the MLR and MNLR models during the validation process under different MT. The MLR model provided better agreement between the measured and calculated θ_v values than the MNLR model. This finding is reflected in the high r (0.87-0.95) and IA (0.89-0.97) values, and the low $RMSE$ (0.24-0.44) values for the MLR model. The MLR model for the NM treatment had 9.32% and 6.84% higher r and IA values, respectively, than the MNLR model, and it had a 6.04% lower $RMSE$ value. The r and IA values for the MLR model in the BPF treatment increased by 2.31% and 2.51%, respectively, whereas the $RMSE$ value decreased by 19.94%. Moreover, r and IA values in the PTW treatment during the validation process increased to 15.08% and 7.76%, respectively, and the $RMSE$ value decreased to 34.21% in the MLR model.

There were considerable differences between the calculated θ_v values for the different MT in the MLR and MNLR models, as shown in Figure 8. The MLR model for the prediction of θ_v with the BPF mulching was the most accurate. The MLR model for the BPF treatment yielded the highest r and IA values and the lowest $RMSE$ value compared with the corresponding values for the NM and PTW treatments. For the BPF treatment, modeling with MLR gave r values that were 8.91% and 1.94% more accurate than those

of the NM and PTW treatments, respectively, and 8.96% and 1.29% more accurate, respectively, for the IA values. The MLR model's BPF had $RMSE$ values that were 44.34% and 19.21% more accurate for θ_v , compared with NM and PTW, respectively. For the PTW treatment, the MLR model produced r and IA values that were 6.84% and 7.57% more accurate, respectively, and 31.11% more accurate for the $RMSE$ values than those obtained for the NM treatment. Hence, the r , IA , and $RMSE$ values for the two models confirmed that the MNLR model performed poorly, whereas the MLR model successfully calculated the θ_v values.



Note: NM: no mulching; BPF: black plastic film; PTW: palm tree waste.

Figure 8 Statistical criteria of coefficients of correlation (r), root mean square error ($RMSE$), and index of agreement (IA) for the regression models during the validation process

4 Conclusions

The effects of different mulching types (MT) in an subsurface drip irrigation (SDI) system on soil water content (θ_v) distribution were investigated. The use of black plastic film (BPF) or palm tree waste (PTW) enhanced the soil's ability to hold water. In the SDI system, BPF mulching required the application of less water than PTW mulching. Therefore, it is recommended that SDI is beneficial to the soil, and when a drip line depth from the soil surface (D_L) of 15 cm is installed and mulching is conducted with PTW, there are no additional costs. This approach expands the active soil zone to the roots of crops. Therefore, the strategy

presented in this study can save water resources in Saudi Arabia's crop fields at a remarkably low cost.

θ_v values were derived as a function of MT, D_L , spacing from drip line, and soil depth, using multiple linear regression (MLR) and multiple nonlinear regression (MNL) analyses. The accuracy of the MLR and MNL models were studied using the coefficients of correlation (r), root mean square errors (RMSE) and index of agreement (IA). Evaluation of the models found that the MLR model fitted well based on the high r and IA values and low RMSE values obtained. The MLR model showed better performance in calculating θ_v values than the MNL model. The MLR model for the BPF treatment was more accurate than no mulching and PTW treatments. Overall, it is concluded that the MLR model can be used to produce accurate outcomes to predict θ_v values.

Acknowledgements

The authors extend their appreciation to the Deanship of Scientific Research at King Saud University for funding this work through research group (No. RG-1440-022).

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